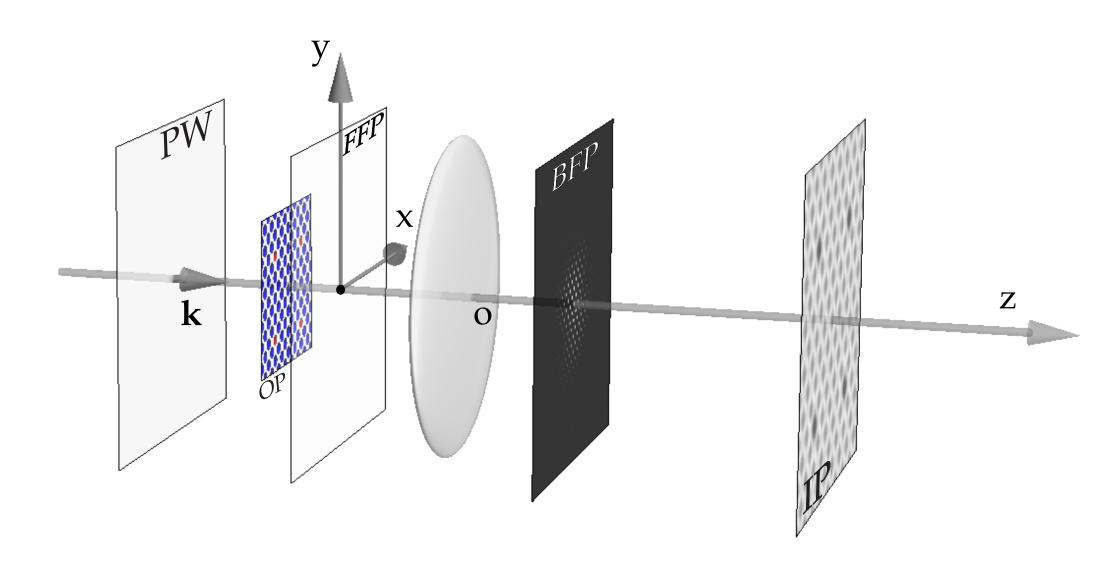
# TEM and STEM Image Simulation

Winter School on High Resolution Electron Microscopy
Held at the
John M. Cowley Center for High Resolution Electron Microscopy
January 2 - 5, 2018

Pierre Stadelmann JEMS-SAAS CH-3906 Saas-Fee Switzerland

December 18, 2017

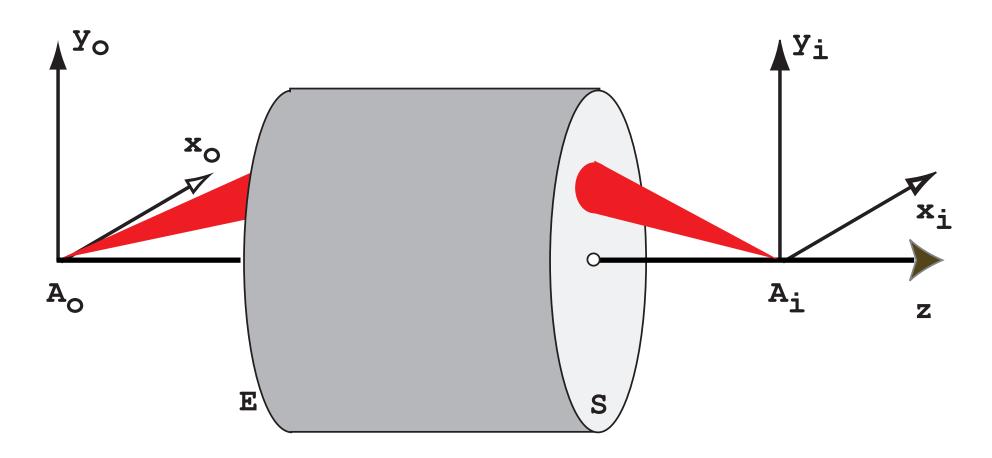
#### TEM: reminder



TEM modelling steps: incident wave (PW), crystal (OP), electron-matter interaction, Fraunhofer approximation, image formation (Abbe theory), ...

- Optical system.
- Aberrations.
- TEM transfer function & STEM: optical transfer function.
- Comparison HRTEM HRSTEM.

## Optical system



An optical system produces the image  $A_i$  of a point source object  $A_o$ .  $A_o$  and  $A_i$  are said to be conjugate.  $A_i$  is not a point since any optical system is diffraction limited. This limitation is introduced by the entrance and exit pupils of the optical system.

#### Transfer function

Optical system as a black box that gives an image wave-function  $\Psi_i(\vec{x})$  of an object wave-function  $\Psi_o(\vec{x})$ :

$$\Psi_i(\vec{x}) = S\{\Psi_o(\vec{x})\}$$

- Linearity.
- Space invariance.

#### Linearity

$$S\{a_1\Psi_o^1(\vec{x}) + a_2\Psi_o^2(\vec{x})\} = a_1S\{\Psi_o^1(\vec{x})\} + a_2S\{\Psi_o^2(\vec{x})\}$$
  
$$S\{a_1\Psi_o^1(\vec{x}) + a_2\Psi_o^2(\vec{x})\} = a_1\Psi_i^1(\vec{x}) + a_2\Psi_i^2(\vec{x})$$

Linearity allows to decompose the object wave-function in a infinite sum of point sources:

$$\Psi_o(\vec{x}) = \int_{-\infty}^{\infty} \Psi_o(\vec{u}) \delta(\vec{x} - \vec{u}) d\vec{u}$$

The image wave-function is then:

$$\Psi_{i}(\vec{x}) = S\left\{\int_{-\infty}^{\infty} \Psi_{o}(\vec{u})\delta(\vec{x} - \vec{u})d\vec{u}\right\} = \int_{-\infty}^{\infty} \Psi_{o}(\vec{u})S\{\delta(\vec{x} - \vec{u})\}d\vec{u} = \int_{-\infty}^{\infty} \Psi_{o}(\vec{u})T(\vec{x};\vec{u})d\vec{u}$$

where  $T(\vec{x}; \vec{u})$  is **Impulse response** of the optical system.



#### Space invariance

#### Space invariance

Space invariance is realised when the image of a point source is independent of its position in the object plane, i.e. when the point source moves in the object plane its image moves similarly in the image plane without changing form and intensity.

$$T(\vec{x}; \vec{u}) = T(\vec{x} - \vec{u})$$

$$\Psi_i(\vec{x}) = \int_{-\infty}^{\infty} \Psi_o(\vec{u}) T(\vec{x} - \vec{u}) d\vec{u} = \Psi_o(\vec{x}) \otimes T(\vec{x})$$

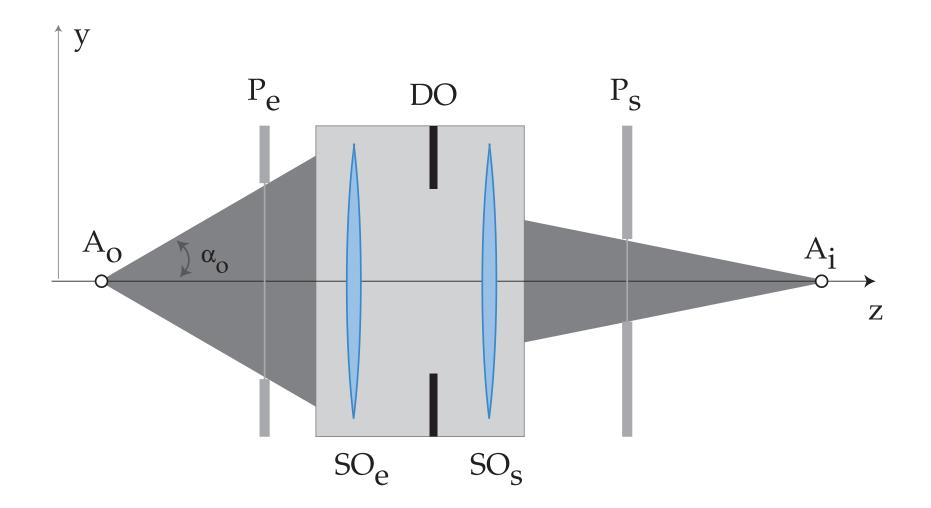
The convolution integral spreads the object information and degrades the performences of the optical system.

Taking its Fourier transform:

$$\widetilde{\Psi}_i(\vec{h}) = \widetilde{\Psi}_o(\vec{h}) \widetilde{T}(\vec{h})$$

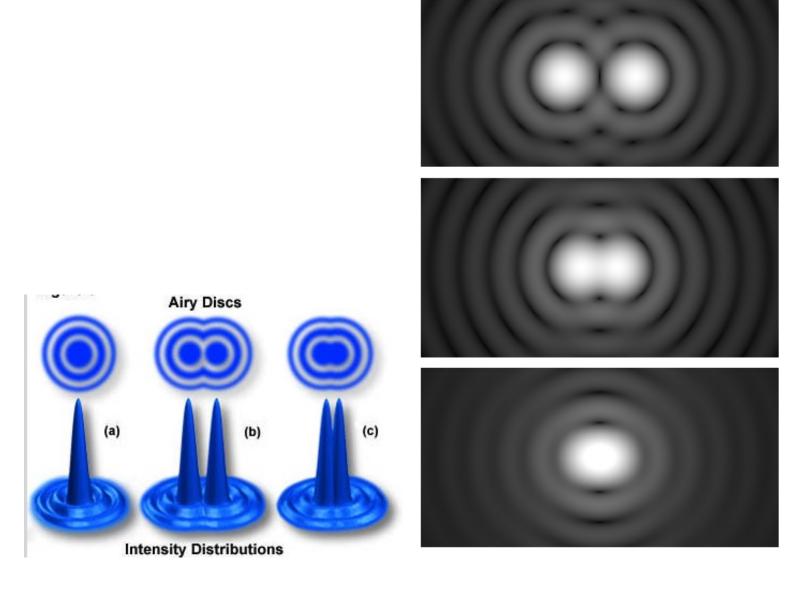
 $\widetilde{T}(\vec{h})$  is the transfer function of the optical system.

#### Pupils



Any optical system can be characterised by an entrance pupil  $P_e$  and an exit pupil  $P_s$ . The pupils are the image of the opening aperture DO by the entrance and exit optical subsystems  $SO_e$  and  $SO_s$ . The portion of the object wave-function accepted by the optical system is limited by the  $P_e$ , while  $SO_s$  limits the extend of the image wave-function. For a perfect optical system, the image of a point source will be an Airy disk.

# Airy disks and Rayleigh resolution criterion



Airy disks.

Airy disks near Rayleigh resolution criterion.

- Optical system.
- Aberrations.
- HRTEM transfer function & HRSTEM: optical transfer function.
- Comparison HRTEM HRSTEM.

#### Aberrations: how to define them

Some light rays emitted by object point  $A_o$  do not reach the image at point  $A_i$ .

Position of  $A_i \longrightarrow$  intersection of the reference light ray (non deviated) and the image plane.

The image of a point source is a **spot** whose shape and intensity depend of the quality of the optical system.

#### Two types of aberrations:

- Monochromatic.
- Chromatic ( $\lambda$  dependent).

#### Monochromatic aberrations

In order to evaluate the monochromatic aberrations one must define a function characteristic of the optical system.

#### This function will depend on:

- The selected reference planes.
- The optical path followed by the light ray.

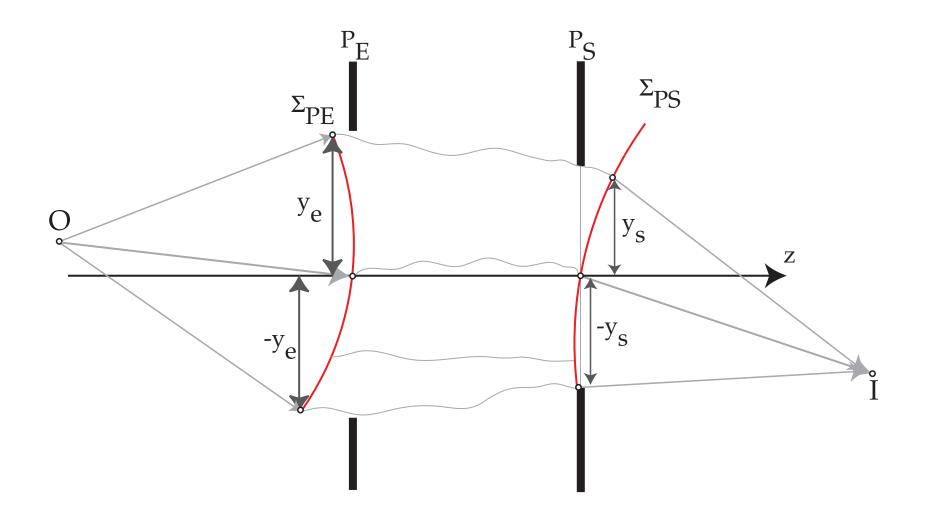
#### Optical path: length

The important feature is the optical path length (OPL).

$$OPL(P_1P_2) = \int_{P_1}^{P_2} n(\overrightarrow{r}) ds$$

- OPL is measured in meters  $(n(\vec{r}) = \frac{c}{v(\vec{r})}$  has no unit).
- OPL is proportional to the time spent by the light ray to travel from  $P_1$  to  $P_2$ .
- OPL is measured from the entrance pupil  $P_E$  to the exit pupil  $P_S$ .

## Optical Path Length: OPL



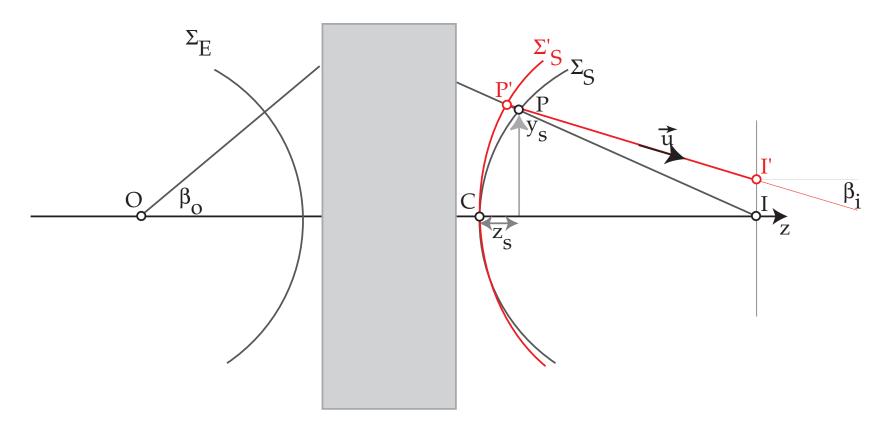
- Before  $P_E$  the reference wavefront  $\Sigma_{PE}$  is spherical (point source at O).
- After  $P_S$  the reference wavefront  $\Sigma_{PS}$  is spherical (converges towards I).

For a perfect optical system, both the entrance  $\Sigma_{PE}$  and exit  $\Sigma_{PS}$  wavefronts are spherical. The Optical Path Length form O to I is independent of the path.

#### Difference of OPL: OPD

The OPD measure the deviation of a wavefront from a perfect spherical wavefront (vacuum or homogenous medium).

At the exit pupil  $P_S$ , the spherical wavefront converging towards I defines the reference wavefront.



In the presence of aberrations the wavefront  $\Sigma_S'$  is no more spherical. The Optical Path Dinference (distance between the deformed  $\Sigma_S'$  and spherical waveform  $\Sigma_S$ ) introduced the phase shift:

$$\delta\phi=e^{2\pi\imathrac{OPD(x_{\mathcal{S}},y_{\mathcal{S}})}{\lambda}}$$

### Transverse geometric aberrations: $\vec{\epsilon}$

The transverse geometric aberrations are proportional to  $\frac{d}{d\theta}$  wavefront aberrations<sup>1</sup>:

$$\epsilon_{x} = -\frac{f}{n_{i}} \frac{\partial W}{\partial x_{s}}$$

$$\epsilon_{y} = -\frac{f}{n_{i}} \frac{\partial W}{\partial y_{s}}$$

f focal length.

The OPD's introduced by all the aberrations of the imaging system are collected in a function  $\chi(\vec{u})$  and the phase shift is<sup>2</sup>:

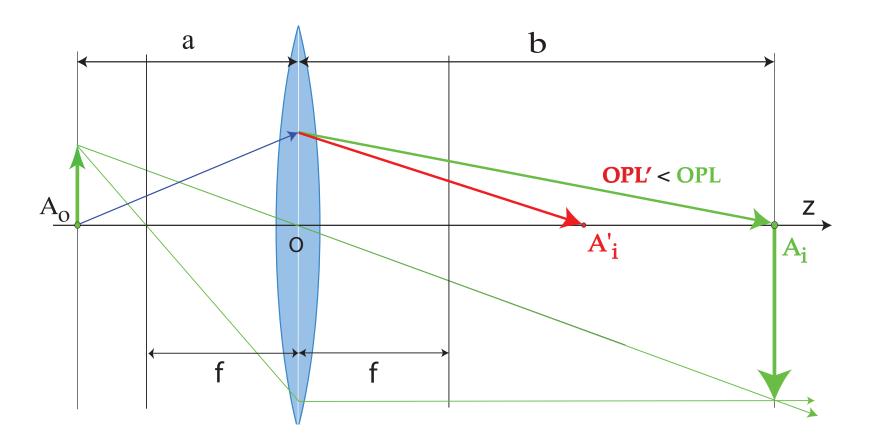
$$\widetilde{T}(\vec{u}) = e^{-\imath \chi(\vec{u})}$$

 $T(\vec{u})$  has been first employed by Abbe in his description of image formation (1866).

 $<sup>^{1}</sup>P(x_{s},y_{s})$  on the spherical reference wavefront can be characterised by the radial angle  $\theta$ .

<sup>&</sup>lt;sup>2</sup>The angle  $\theta$  corresponds (through Bragg law) to a spatial frequency  $\vec{u}$ , i.e. a distance in the back focal plane.

#### OPD: spherical aberration

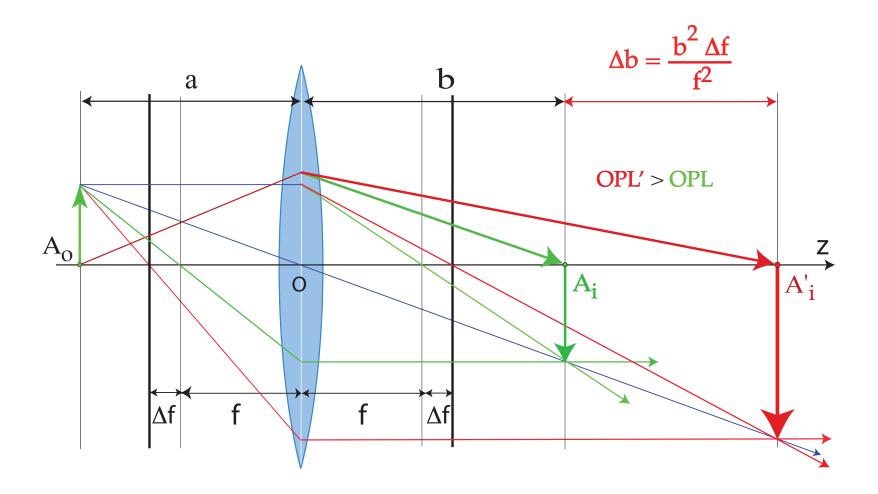


In presence of spherical aberration, the optical path length (OPL') form  $A_o$  to  $A'_i$  is smaller than OPL from  $A_o$  to  $A_i$ . The wavefront at  $A'_i$  is out-of-phase by<sup>3</sup>:

$$e^{-2\pi i \frac{C_s \lambda^3 (\vec{q} \cdot \vec{q})^2}{4}}$$

<sup>&</sup>lt;sup>3</sup>With our plane wave choice  $e^{2\pi i \vec{q} \cdot \vec{r}}$ .

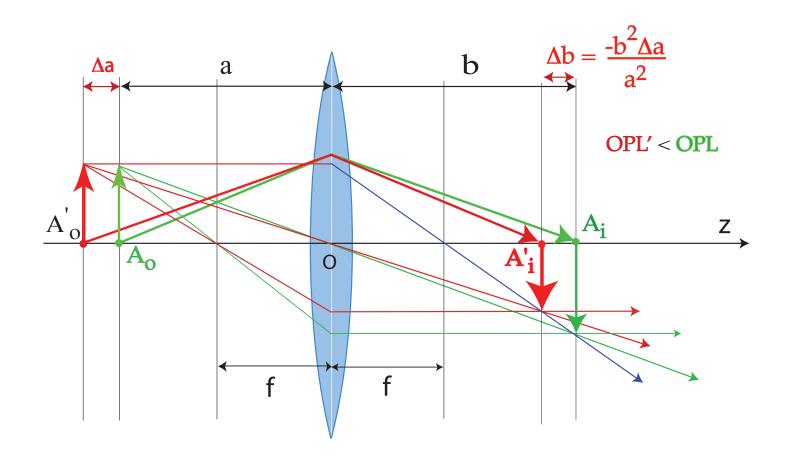
## OPD: underfocus



Underfocus weakens the objective lens, i.e. increases  $\mathbf{f}$ . As a consequence the OPL from  $A_o$  to  $A_i'$  is larger:

 $e^{2\pi i \frac{\Delta f \lambda(\vec{q} \cdot \vec{q})}{2}}$ 

#### OPD: eccentricity



On the contrary keeping  ${\bf f}$  constant and moving the object by  $\Delta a$  decreases the OPL.

# Transfer function $T(\vec{q})$

$$\widetilde{T}(\vec{q}) = e^{-\chi(\vec{q})} = \cos(\chi(\vec{q})) - i\underbrace{\sin(\chi(\vec{q}))}_{\text{CTF}}$$

$$\chi(\vec{q}) = \pi \left[ -W_{20} \lambda (\vec{q}.\vec{q}) + W_{40} \frac{\lambda^3 (\vec{q}.\vec{q})^2}{2} + \dots \right]$$

#### Where:

- *W*<sub>20</sub> : defocus (z)
- $W_{40}$ : spherical aberration ( $C_s$ )

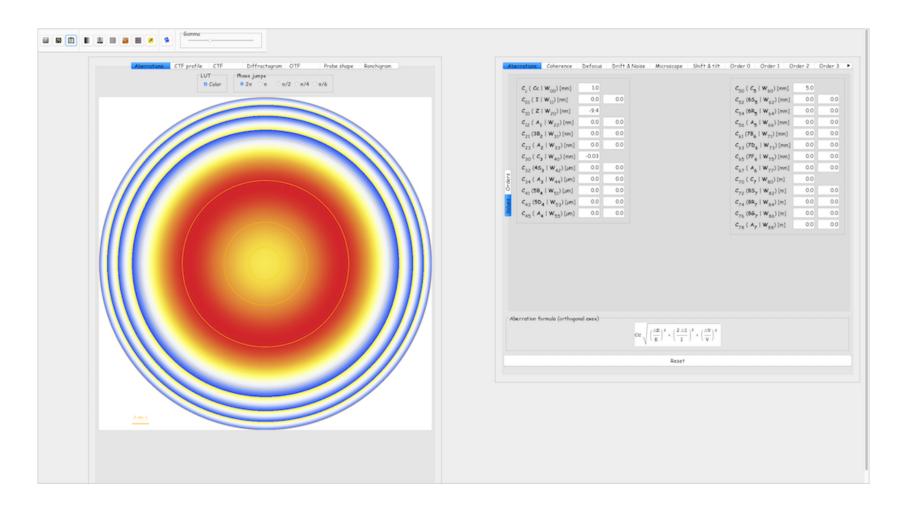
At present TEM and STEM aberration correctors only correct axial aberrations, i.e. aberrations that affect images of point sources located on the optical axis.

## Wavefront aberrations to $6^{th}$ order (cartesian coordinates)

```
\{z, \pi (u^2 + v^2) \lambda\} (defocus)
\{W(1,1), 2\pi(u\cos(\phi(1,1)) + v\sin(\phi(1,1)))\}
\{W(2,2), \pi\lambda((u-v)(u+v)\cos(2\phi(2,2))+2uv\sin(2\phi(2,2)))\}
\{W(3,1), \frac{2}{3}\pi(u^2+v^2)\lambda^2(u\cos(\phi(3,1))+v\sin(\phi(3,1)))\}
 W(3,3), \frac{2}{3}\pi\lambda^2(u(u^2-3v^2)\cos(3\phi(3,3))-v(v^2-3u^2)\sin(3\phi(3,3)))
 W(4,0), \frac{1}{2}\pi (u^2 + v^2)^2 \lambda^3  (3<sup>rd</sup> order spherical aberration or C_3)
 W(4,2), \frac{1}{2}\pi(u^2+v^2)\lambda^3((u-v)(u+v)\cos(2\phi(4,2))+2uv\sin(2\phi(4,2)))
 W(4,4), \frac{1}{2}\pi\lambda^3((u^4-6v^2u^2+v^4)\cos(4\phi(4,4))+4u(u-v)v(u+v)\sin(4\phi(4,4)))
 W(5,1), \frac{2}{5}\pi (u^2 + v^2)^2 \lambda^4 (u\cos(\phi(5,1)) + v\sin(\phi(5,1)))
 W(5,3), \frac{2}{5}\pi(u^2+v^2)\lambda^4(u(u^2-3v^2)\cos(3\phi(5,3))-v(v^2-3u^2)\sin(3\phi(5,3)))
 W(5,5), \frac{2}{5}\pi\lambda^4 \left(u\left(u^4-10v^2u^2+5v^4\right)\cos(5\phi(5,5))+v\left(5u^4-10v^2u^2+v^4\right)\sin(5\phi(5,5))\right)
  W(6,0), \frac{1}{3}\pi \left(u^2+v^2\right)^3 \lambda^5 \left. \left\{ (5^{th} order spherical aberration or C_5) \right. \right.
  W(6,2), \frac{1}{3}\pi (u^2 + v^2)^2 \lambda^5 ((u-v)(u+v)\cos(2\phi(6,2)) + 2uv\sin(2\phi(6,2)))
 \{W(6,4), \frac{1}{3}\pi\lambda^5((u^6-5v^2u^4-5v^4u^2+v^6)\cos(4\phi(6,4))+4uv(u^4-v^4)\sin(4\phi(6,4)))\}
\{W(6,6), \frac{1}{2}\pi\lambda^5((u^6-15v^2u^4+15v^4u^2-v^6)\cos(6\phi(6,6))+2uv(3u^4-10v^2u^2+3v^4)\sin(6\phi(6,6)))\}
```

jems describes wavefront aberrations to order 8 <sup>4</sup>.

#### Wave-front aberrations to order 8



Wave-front aberrations up to order 8 can be introduced in HRTEM image formation and HRSTEM probe formation.

- Optical system.
- Aberrations.
- HRTEM transfer function & HRSTEM: optical transfer function.
- Comparison HRTEM HRSTEM.

# Transfer Function $T(\vec{u})$ and Optical Transfer Function $OTF(\vec{u})$

#### **HRTEM**

coherent or partially coherent image formation process with coherent or partially coherent incident wave.

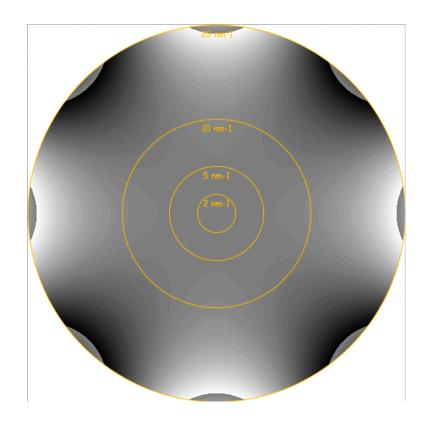
#### **HRSTEM**

incoherent image formation process with coherent or partially coherent probe.

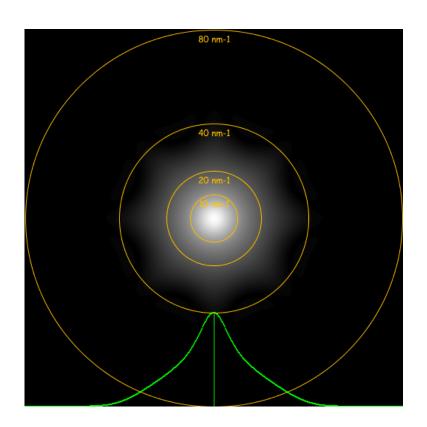
Probe function  $P(\vec{x})$ : source intensity distribution as measured at the sample plane.

### HRTEM / HRSTEM problem: aberrations of optical system

Reaching 0.05 nm resolution sets very strong conditions on aberrations correction.



Aberration figure of  $C_{34}(0.5\mu\mathrm{m})$ , phase jump at  $\frac{\pi}{4}$ .



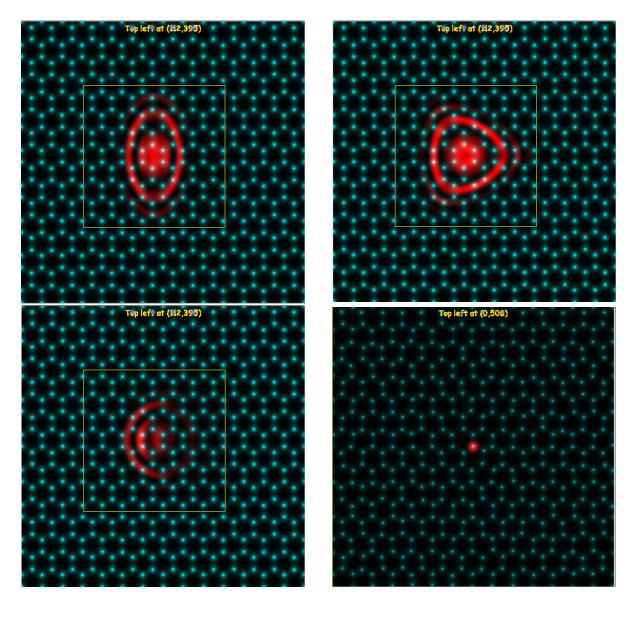
Optical Transfer Function.

Note that Optical Transfer Function (HRSTEM) transfers higher spatial frequencies than Ccoherent Transfer Function (HRTEM).

## $P(\vec{x})$ : source intensity distribution as measured at the sample plane

2 fold astigmatism.

3 fold astigmatism.



Coma.

Corrected probe.

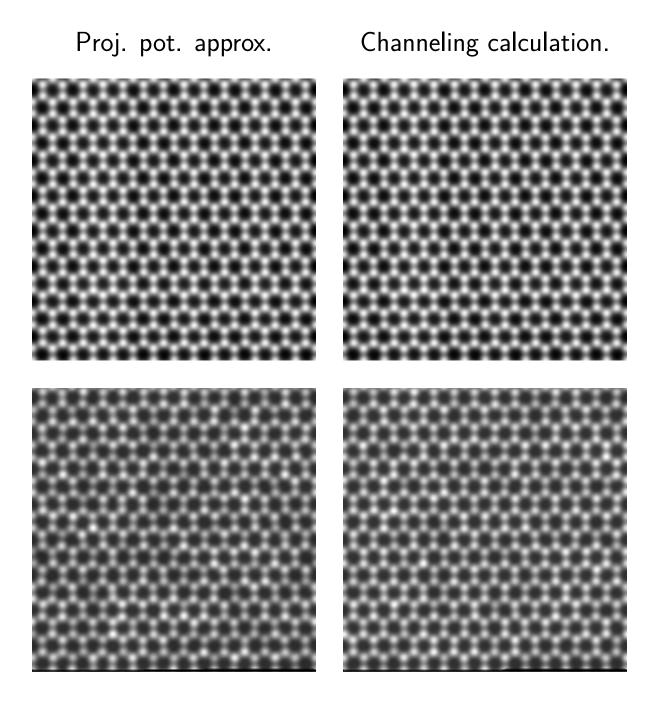
## STEM imaging: calculating $I_0(\vec{x})$

Numerous approximations are involved in calculating  $I_0(\vec{x})$ :

- Simple projected potential + convolution with probe intensity: no channeling effect (Weak Object Approximation).
- ullet Multislice calculation: channeling + inelastic scattering (absorption or optical potential) + convolution with probe intensity.
- Frozen lattice (phonon) approximation: atoms of super-cell displaced out of equilibrium position, probe scanned on imaged area, intensity collected by annular detector. Allows to simulate HAADF (High Angle Annular Dark Field), BF (Bright Field), MAADF (Medium Angle Annular Dark Field), DPC (Differential Phase Contras), ...
- Pennycook, Nellist, Ishizuka, Shiojiri, Allen, Wang, Rosenauer, van Dyck, ...

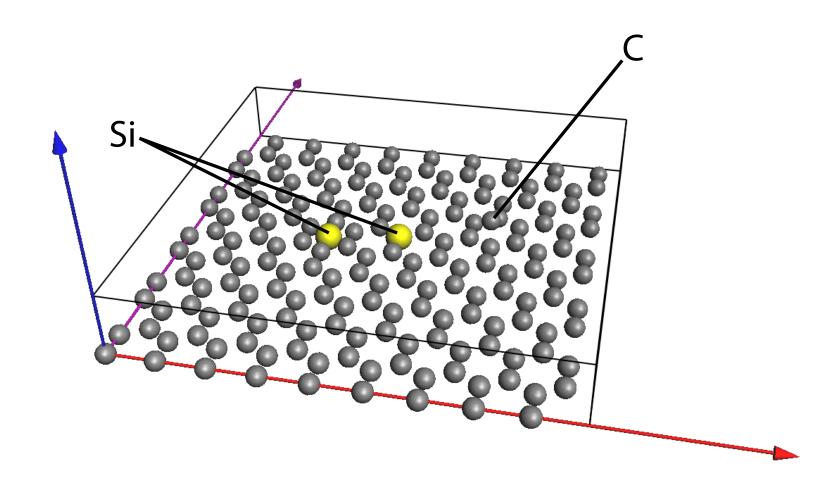
Except the first 2 methods, usually rather long simulation time (faster calculations using GPU).

# STEM imaging: graphene



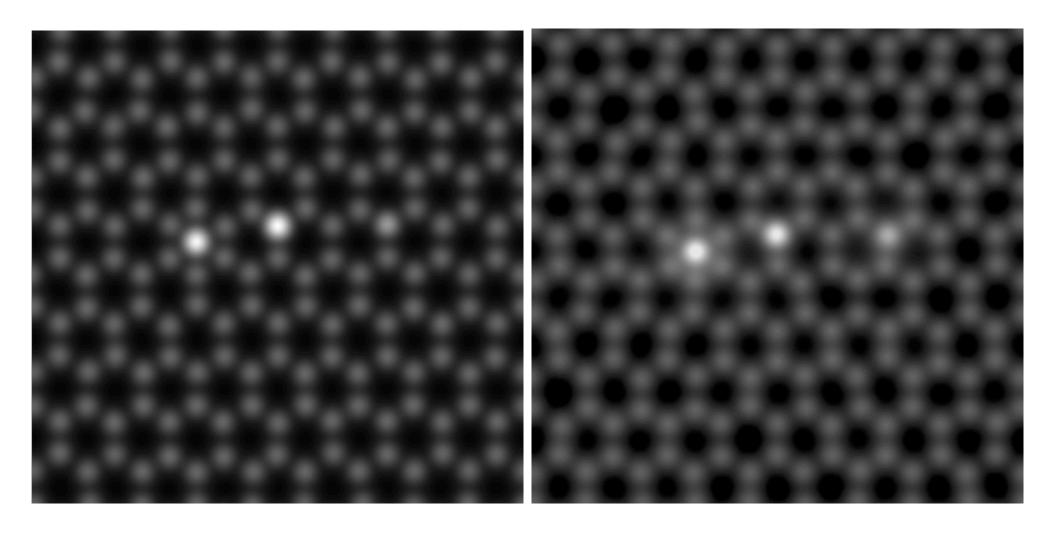
- Optical system.
- Aberrations.
- HRTEM transfer function & HRSTEM: optical transfer function.
- Comparison HRTEM HRSTEM.

# HRSTEM - HRTEM comparison: graphene with add atoms



Graphene with Si in 6 C ring, Si substitutional and 2 C column.

## Graphene: HAADF (100 kV, 70 -150 mrad)

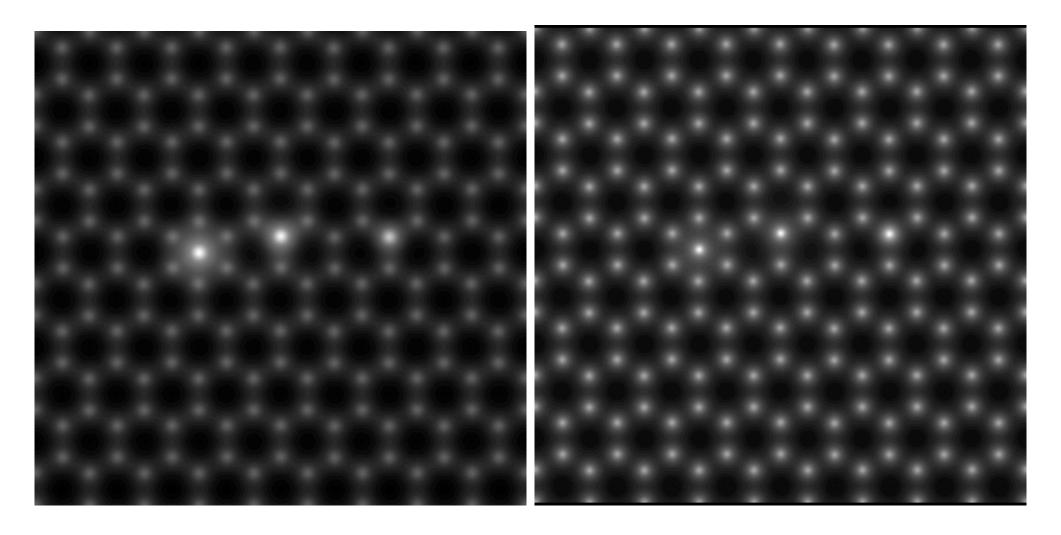


Frozen lattice ( $\sim$ 400 s).

Channeling ( $\sim$ 2 s).

One Si shows more contrast than 2 C atoms (i  $\sim$   $Z^2$ ) : 14<sup>2</sup> compared to  $\sim$  2  $\times$  6<sup>2</sup>.

## Graphene: HRTEM (100 kV, $C_s - 0.033mm$ )



Weak phase object app.,  $C_c = 0.5mm$ 

Multislice,  $C_s = -0.033mm$ ,  $C_c = 0$ , no thermal magnetic noise.

HRTEM does not display the strong contrast difference between one Si and two C as given by HAADF.

# Thanks for your attention!